

Chemical Process Safety: Which parameters are important to perform a chemical reaction in a safe way?

(Presentation by Dr Stefan Gries, Boehringer Ingelheim Corporate Center)

Speaker: Liu Li (刘立) EHS&S China, Boehringer Ingelheim

AGENDA 大纲

- 1. Session 1
- Process safety parameters
- Essential information to chemical processes
- Critical interactions of material
- Exothermic and run-away reaction
- Scale up
- 2. Session 2
- Runaway reaction
- PSCI Questionnaire & Typical Observations
- 3. Audience questions & discussions



Mr. Liu Li

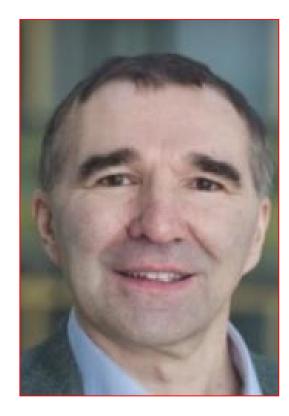
- Chemist
- 13 years in Pharam Industry
- 8 years with Boehringer Ingelheim China
- Current position: EHS & S Manager
- Former positions in
 - Medicinal Chemsitry
 - Chemcial Process Research and Development
 - EHS&S

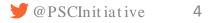




Dr. Stefan Gries

- Chemist
- More than 25 years with Boehringer Ingelheim
- Current position: Corp. EHS & S (occupational health, exposure control, soil and groundwater protection, EHS auditor)
- Former positions in
 - Local EHS (Safety Engineer)
 - Research & Development (Head of pilot plant)
 - Chemical Production (Head of production plant)

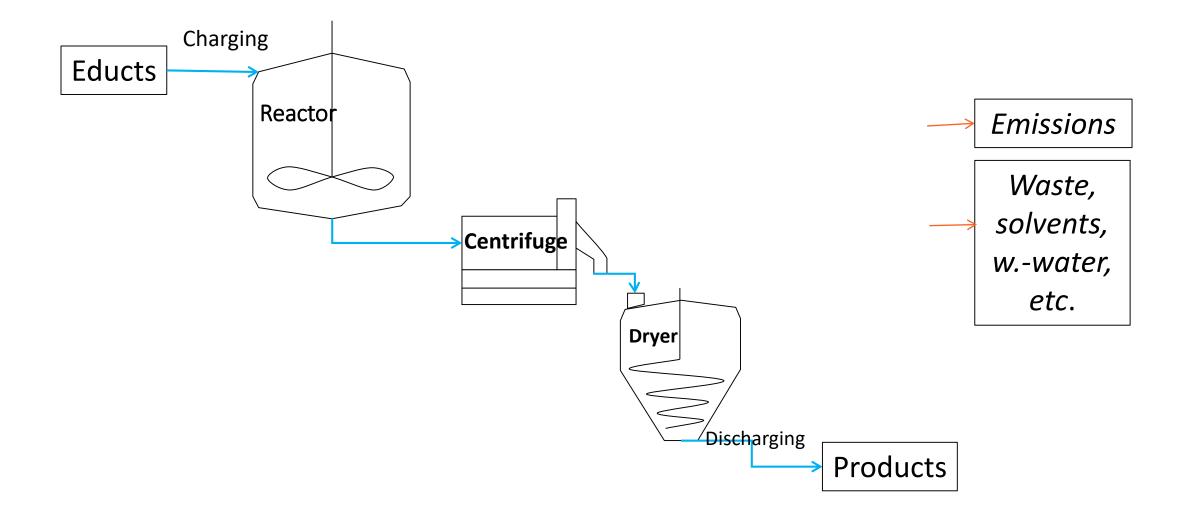




TRAINING STRUCTURE

- 1. Session 1
- Process safety parameters
- Essential information to chemical processes
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Chemical reaction in a production plant





Which information is necessary for a safe process?

- Knowledge about the used chemicals regarding thermal stability, physical safety parameters and toxicology
- Educts
- Products (incl. side products)
- Reagents
- Solvents & Auxiliaries
- Knowledge about the chemistry
- Main reaction and side reactions
- Waste streams (gas release, liquids and solids)
- Consecutive reaction, decomposition?
- Reaction type
- Batch reaction
- Semi-batch reaction
- Continuous flow reaction



- Calorimetric data of the chemical reaction
 - Adiabatic temperature rise
 - Gas evolution rate (\rightarrow reactor venting sufficient?)
 - precipitation of solids (\rightarrow reduction of heat transfer, stirrer blocking?)
 - Accumulation of reactants, thermal output/time
 - Stability of reaction mixtures, distillation residues, etc.
 - Potential for runaway reaction, abnormal operating conditions
 - If necessary: investigation of the runaway reaction
- Knowledge about critical interaction between the used chemicals and other material
 - Material resistance of reactor & other equipment
 - Possible material contact (e.g. media supply)

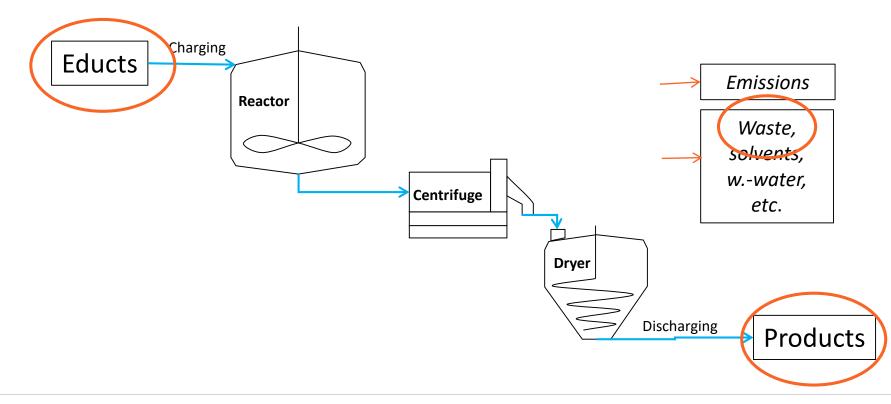
- Plant equipment "state of the art"
 - Materials of the equipment = > material tests, corrosive data, etc.
 - Inertisation of equipment
 - Earthing of the equipment, explosion-proof equipment
 - Blow-down system, pressure relief valve, rupture disc,
 - Heating and cooling medium & capacity
 - Safety concept e. g. for electrical shut down
- → Process Hazard Analysis

Examination of the chemical properties and chemical process safety data together with the technical installation of the plant.

A safe chemical process is always an adequate combination of safe substance handling, known chemical process and adapted equipment.



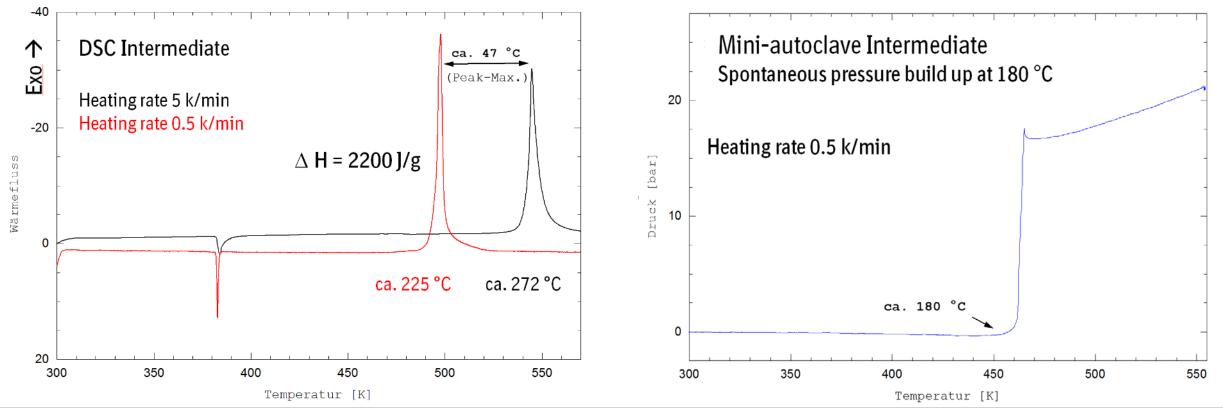
Thermal stability of chemical substances and reaction mixtures





Thermal stability of chemical substances and reaction mixtures

- Thermal stability:
 - Differential Scanning Calorimetry (DSC) or Differential Thermo Analyses (DTA)
- Decomposition test closed vessel (pressure build-up):
 - e.g. in a mini-autoclave



Known hazardous substances

Typical chemical functions in thermodynamically unstable compounds:

- acetylene and acetylide -CEC-azide and hydrogen azide $-N_3$ diazonium salts, triazene, tetrazene -NEN+ -N=N-azo compounds -HN-NHhydrazide fulminates, oximates >C=N=O halogene nitrogene compounds >N-X $-NO_{x}$ nitrites, nitrates, nitro- and nitroso compounds peroxides, peroxy acids, ozonids -0-0-
- -O-ClO_x (per-)chlorate, (hypo-)chlorite

Known highly reactive substances

- Typical compounds or chemical functions:
 - R-Mg-X Grignard reagents
 - R-Li
 - -COCI acid cloride
 - -CO-O-OC- acid anhydride

organic lithium compounds

Sodium-, Potassium alkoholate

inorganic anhydride

conc. acids, lyes

hydride

- Na-, K-OR
- $POCl_3, SOCL_2$
- "H₂SO₄"

PSCI

- NaH, LiAlH₄
- Na, K, Mg, Li ... metals
- O_2 , H_2 gases • F_2 , Cl_2 , Br_2 halogen

General handling characteristic of substances

- Additional test for thermal stability
 - Thermogravimetry (TG) or combination TG/DSC; TG/DTA
 - Quasi-adiabatic heat aging in a Dewar flask (or an adiabatic calorimeter)
 - Time Pressure Test
- Flammability of solids or liquids
 - Combustion test
 - Flammability of solids
 - Smoldering temperature; minimum ignition temperature of a dust layer
 - (minimum) dust cloud ignition temperature
 - Ignition temperature of liquids
 - Flash point (of liquids)



General handling characteristic of substances

- Dust explosibility:
 - Dust explosion test
 - Dust explosion characteristics (p_{max}; (dp/dt)_{max}; K_{st}; explosion limits
 - Minimum ignition energy (MIE)
- Mechanical sensitivity, further safety characteristics
 - Sensitivity to impact
 - Sensitivity to friction
 - Self-ignition test
 - Conductivity





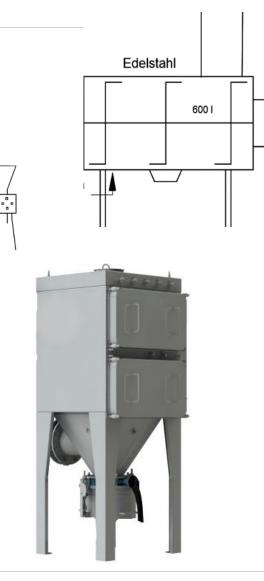
Details to: Dust stability/explosibility

- Mechanical sensitivity: Sensitivity to impact / friction
- Important for mechanical actions

 (e.g. transport systems, in dryer with agitator, in a pin mill,)
 maximum temperature & agitation time
- Maximum explosions pressure p_{max}

For most of the organic gases and vapors in mixture with air p_{max} is between 8 bar to 10 bar under initial atmospheric conditions.

- Important for e.g. venting pipes/filter units, for mills, dryers ("dust containing air")
 - ightarrow explosion-resistant design



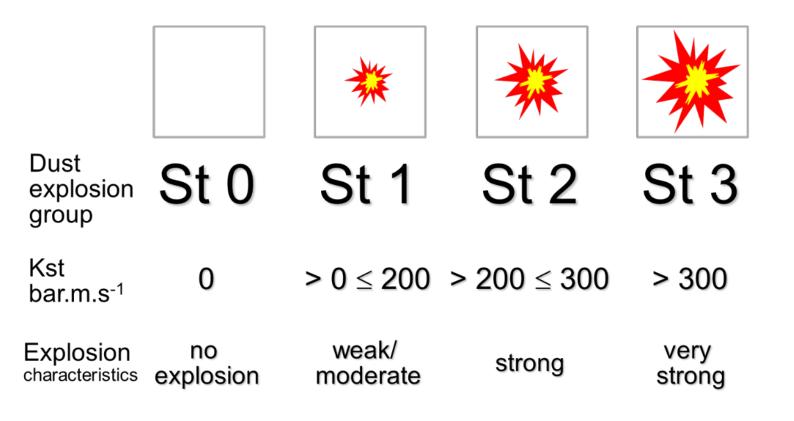
Details to: Flammability of solids or liquids

Ignition temperature

Auto-ignition temperature (according to EN 14 522)	Temperature class	Maximum surface temperature
> 450 °C	Τ1	450 °C
> 300 °C to 450 °C	Т 2	300 °C
> 200 °C to 300 °C	Т 3	200 °C
> 135 °C to 200 °C	Т 4	135 °C
> 100 °C to 135 °C	Т 5	100 °C
> 85 °C to 100 °C	Т 6	85 °C

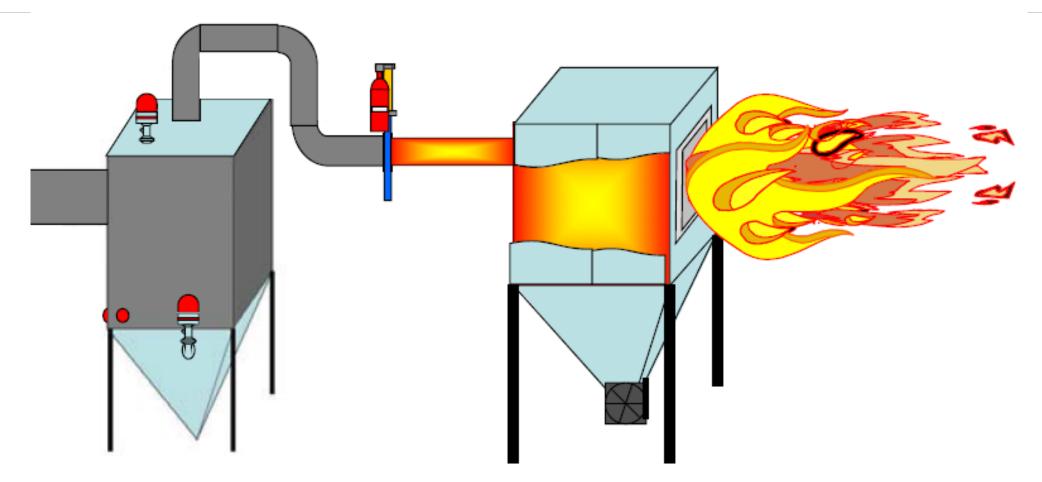
Details to: Dust explosibility

Maximum explosion pressure rise (dp/dt)_{max} and K_{st}



Important for design of "explosion relief", "explosion suppression" system

Examples of Process Equipment



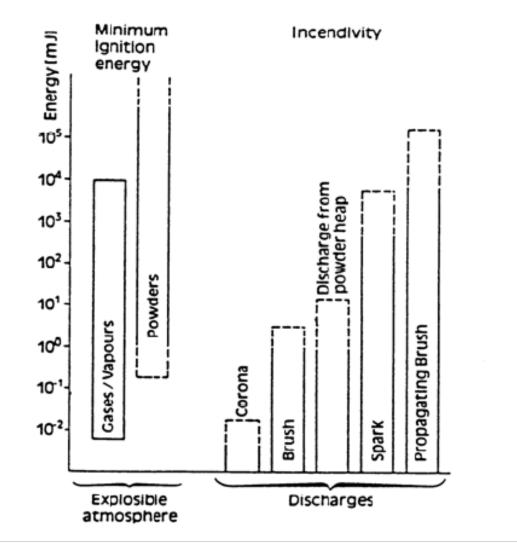
 \blacktriangleright If the K_{st} is above 300 bar m/s, the valve would not work



Details to: Dust explosibility

Minimum ignition energy (MIE)

Risk	Substance Name	MIE in air	
	Hydrogen	0.01mJ	
	Methanol	0.14 mJ	
High risk	n-HeptanE	0.24 mJ	
< 25 mJ	Acetone	1.15 mJ	
	"Normal organic" dust	>10 mJ	
	Paracetamol	<10 mJ	
	Wheat flour	~50 mJ	
Medium risk 25 – 100 mJ	Sugar powder	30-100 mJ	
25 – 100 mj	Coal	30-100 mJ	
Low risk >100 mJ	PVC	1500 mJ	

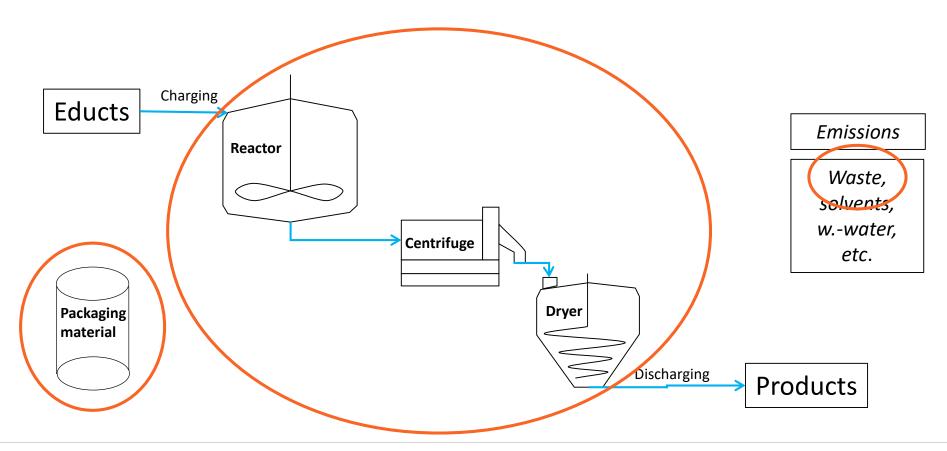


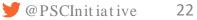
Resulting technical requirements of equipment

Temperatur Class										
Explosion T1		T1	T2	T3	T4	T5	Т6			
Group		(>450°C)	(> 300°C)	(> 200°C)	(> 145°C)	(> 100°C)	(> 85° C)			
IIA			Acetone	Fuel	Hexane	Acetal- dehyde				
	MIF	ļ	Acetic acid	Methanol	Diesel					
	2	-	Methane	Butan	Fuel oil					
			Propane							
			Ammonia							
			Benzene							
			Toluene							
IIB			Hydrogen	Ethanol	Hydrogen					
			cyanide	Ethane	sulfide					
IIC			Hydrogen					Carbon disulfide		



Critical interaction between the used chemicals and between chemicals and materials





Critical interaction between chemicals and materials

- Incident in a chemical production plant
- Due to an operational error a mixture of thionyl chloride, ethyl acetate and acetyl chloride have to be disposed of. For disposal the worker used the empty thionyl chloride drum. Short time later the drum exploded.
- Result of safety examination in laboratory
- No critical reaction between thionyl chloride, ethyl acetate and acetyl chloride.
- But, the used drum was zinc-coated
 → critical reaction under pressure build-up between ethyl acetate, thionyl chloride and zinc !



Critical interaction between chemicals and materials

- Incident in a chemical production plant B:
- In a process the excess of POCl₃ is distilled off and purged into a 200 l steel drum with a PE-inliner. Approx. 10 h later the drum burst.
- Between the batches the pipes were washed with acetone. Residual quantities of acetone remained in the pipes.
- Result of safety examination in laboratory:
- Retarded critical reaction between acetone and POCl₃.

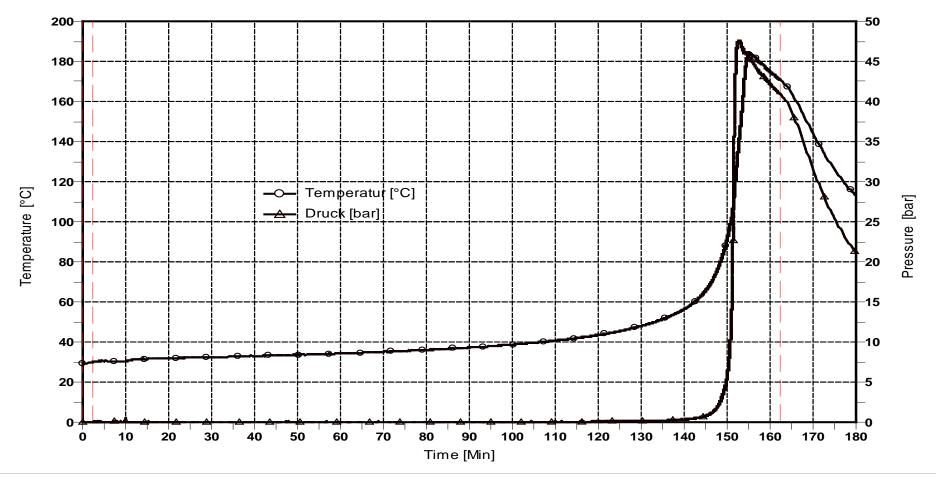






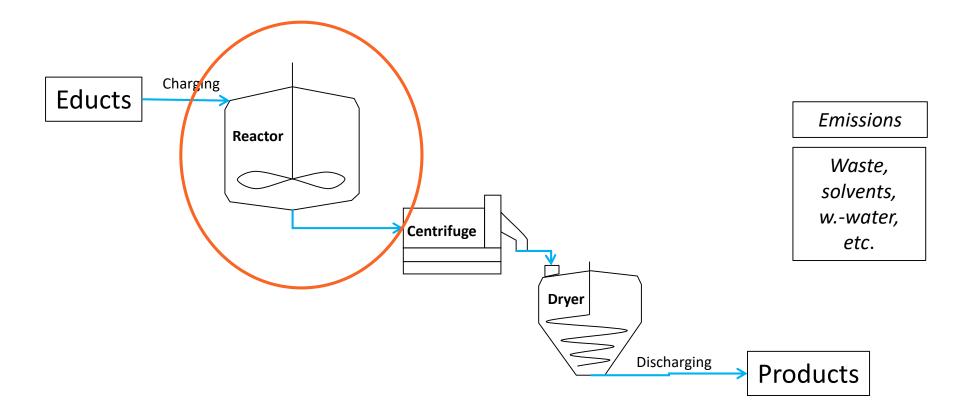
Critical interaction between chemicals and materials

- Reaction experiment
- closed cell test, POCl₃ overlay with ca. 5.8 weight-% acetone



Chemistry – chemical reaction

Calorimetric measurements for chemical reactions





Chemistry – chemical reaction

- The chemical reaction should be known, including side reactions and consecutive reaction. The chemical reaction can depend on the reaction temperature or the working procedure.
- Mass balance of the whole reaction is very useful
- Side products can have a big influence on process safety
- Are decomposition reactions known?
- Waste streams can contain highly reactive compounds or unstable substances (e. g. slow gas generation leading to a pressure build up in waste containers)

Working procedure for chemical reaction

Batch reaction:

All reagents are charged to the reactor. Then the content is heated to the reaction temperature.

- The accumulation of reaction partners is at the beginning 100 %.
- For an exothermic reaction, if the cooling capacity is not sufficient, an uncontrolled temperature rise occurs and a run away reaction is possible.
- Batch reactions should only be applied with endothermic or very slow reaction with smooth exothermic behavior.

What is in general the best temperature for running a exothermic batch reaction? The lowest possible reaction temperature is in general the safest temperature!



Working procedure for chemical reaction

Semi-batch reaction

One reaction compound (including solvent) is charged to the reactor. The other compound is added over a defined time at the reaction temperature.

- The accumulation of reaction partners is at the beginning 0 %. Across the whole addition time the accumulation should be small.
- Always add the reactive compound. (Adding a catalyst or a compound in a huge excess is not a semi-batch process!)
- A stop of the addition stops further heat generation (if low accumulation).

What is in general the best temperature for running a exothermic semi-batch reaction? The highest possible temperature is the best! -> fast reaction -> less accumulation

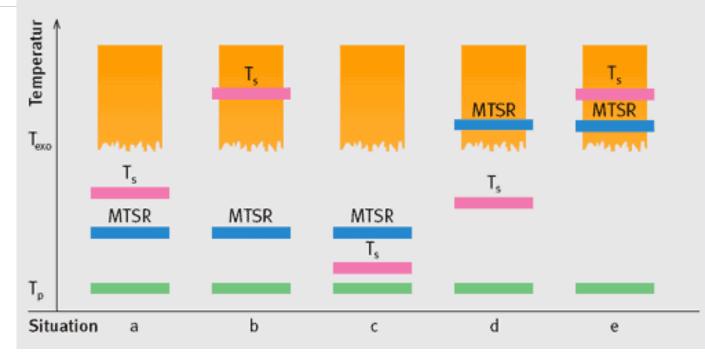


Chemical reaction parameters, calorimetric measurements

- Safety investigation of reaction under process like conditions:
- Reaction calorimeter (e.g. Mettler RC1) with dosing, gas measurement etc.
- Determination of:
- Heat of reaction ΔH_R [J/g] or [J/mol]
- Heat capacity c_p [J/g K]
- Adiabatic temperature rise ΔT_{ad} [K] or [°C]
- Degree of accumulation [%]
- Gas release [l/min]
- Adiabatic investigation of abnormal operating conditions:
- Determination of thermal stability under adiabatic conditions (no heat exchange, like DTA)



Thermal hazard potential of chemical reactions



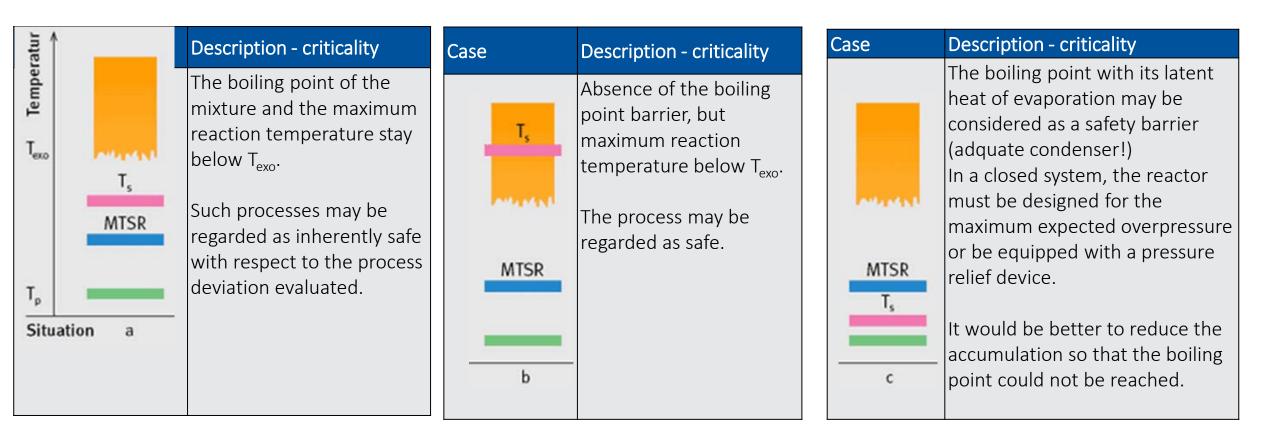
 T_p : process temperature at the start of the deviation

MTSR: maximum temperature of the synthesis reaction; MTSR = T_p + Δ T_{ad} · α_{accu}

- T_{exo}: the maximum temperature at which a substance or reaction mixture can just be handled safely
- T_s : (= T_b) the boiling point in an open system

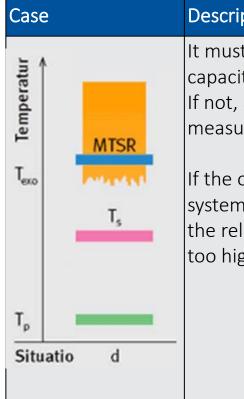


Thermal hazard potential of chemical reactions





Thermal hazard potential of chemical reactions



Description - criticality

It must be evaluated if the evaporation capacity provides sufficient safety. If not, additional organizational or technical measures have to be implemented.

If the operation is performed in a closed system, the temperature corresponding to the relief valve's set pressure may not be too high.

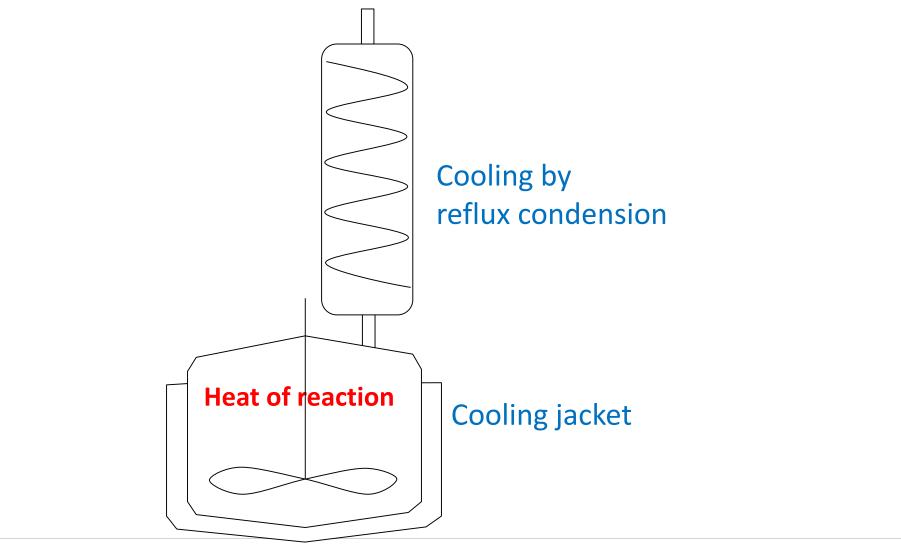


Description - criticality

This case must be rated as problematic. In case of a (simple) cooling failure, the reaction can pass over the safe temperature range.

Plant and/or process modifications should be evaluated in such situations.

Temperature control of chemical reaction





Heat balance of exothermic reactions

heat production



heat removal

Increased heat production

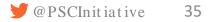
- Additional energy supply (e.g. heating, stirring, pumping)
- Higher concentration of reactants (e. g. missing solvent)
- Presence of a catalyst (e.g. rust, nonferrous metals)
- Initiation of other exothermic processes
 - (e.g. side reaction, decomposition)

Decreased heat removal

Loss of cooling

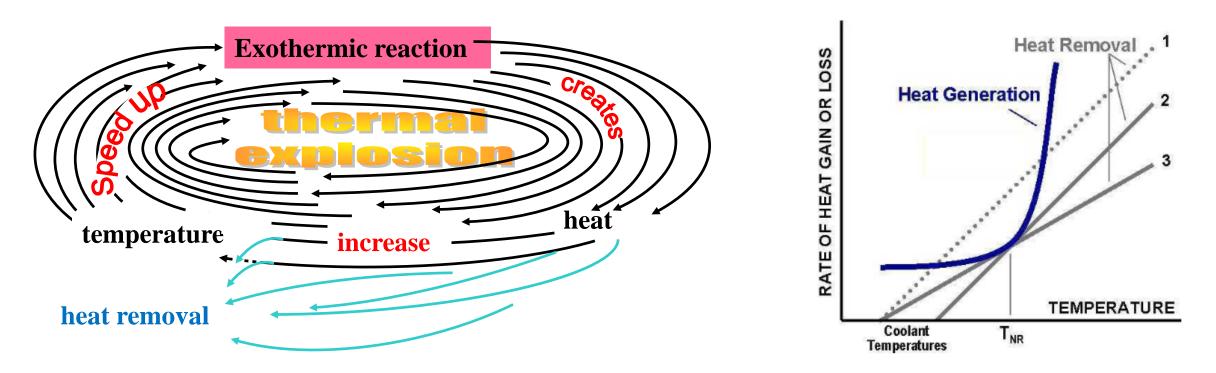
(e.g. pump failure, solvent evaporated)

- Degrade heat transfer (e.g. fouling, adhesion)
- Increase of viscosity (e.g. higher degree of polymerization)
- Inadequate mixing (e.g. pump failure, solvent evaporated, stirrer failure)



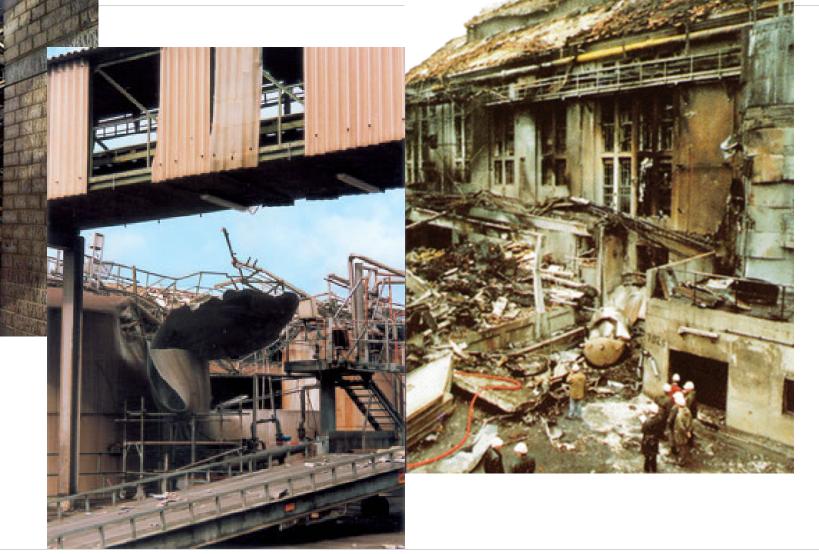
Exothermic and run-away reaction

- An exothermic reaction produces heat which leads to an increase of the reaction temperature if the cooling capacity is not sufficient.
- A runaway reaction is an exothermic chemical process, which leads to uncontrollable reaction conditions due to an uncontrolled rise of the reaction speed.



Exothermic reaction and run-away reaction

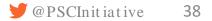






What is necessary for a safe process?

Scale up Reactor Centrifuge Dryer Production Laboratory



Scale up laboratory \rightarrow (pilot) plant

- Example of a heat balance change during the scale up
- From laboratory (1 l) to pilot plant (1 m³).
- Dosing controlled reaction
- Exothermic reaction
- Reaction heat of 360 kJ kg⁻¹ (= 0,1 kWh kg⁻¹)
- Density of reaction mass is 1 g cm⁻³
- Reaction temperature 80 °C
- Filling degree is 100 %
- Heat transmission of both apparatus are 500 W m⁻² K⁻¹
- Effective temperature difference for cooling is 30 K





Scale up – laboratory – (pilot) plant

	Laboratory	Pilot or production plant	
Reactor size	11	1 m ³	Factor 1000
Cooling surface	0,046 m ²	4,4 m ²	Factor ~100
Specific cooling power	15 kW m ⁻² (= 5	600 W m ⁻² K ⁻¹ * 30 K)	
Cooling power	0,69 kW (= 15 kW m ⁻² * 0,046 m ²)	66 kW (= 15 kW m ⁻² * 4,4 m ²)	Factor ~100
Reaction power with 3 h dosing time	0,03 kW (= 0,1 kWh kg ⁻¹ * 1 kg /3h) <i>heating required</i>	33 kW (= 0,1 kWh kg ⁻¹ * 1000 kg /3h) cooling sufficient	
Reaction power with 2 h dosing time	0,05 kW (= 0,1 kWh kg ⁻¹ * 1 kg /2h) <i>no cooling required</i>	50 kW (= 0,1 kWh kg ⁻¹ * 1000 kg /2h) cooling sufficient	
Reaction power with 1 h dosing time	0,1 kW (= 0,1 kWh kg ⁻¹ * 1 kg /2h) cooling sufficient	100 kW (= 0,1 kWh kg ⁻¹ * 1000 kg /1h) cooling insufficient	



Expectation of an EHS auditor

$R&D \rightarrow scale up \rightarrow production$

Amounts of substances	Location	Working documents	Guidance documents
miligrams to grams	Research & Development Laboratory	 Lab documentation First observations to process safety 	 Policy "Safe Research & Development" Lab safety SOPs
grams to kilograms	Transfer from tab to kilolab / pilot plant	- Basic safety report - Transfer report	 Regulation to "Basic safety examinations" Transfer protokoll
kilograms	kilolab / pilot plant	 Batch records Safety assessments Process safety examinations 	 Guidelines for safety examinations SOPs to substance handling etc.



Expectation of an EHS auditor

R&D \rightarrow scale up \rightarrow production

Amounts of substances	Location	Working documents	Guidance documents
kilograms to tons	Transfer from pilot plant to production	- Transfer report - Risk assessment - Technical measures	 Transfer protokoll SOP "Risk assessement/ HAZOP"
kilograms to tons	Production plant	 Batch records Change Control documents Maintenance of technical installation 	- SOP " CC" - SOPs "Maintanance"
kilograms to tons	Transfer to other plants	- Transfer report - Risk assessment - Technical measures	- Transfer protokoll



Usefull Links/ Infos

- https://www.bgrci.de/fachwissen-portal/topic-list/hazardous-substances/
- <u>https://downloadcenter.bgrci.de/resource/downloadcenter/downloads/R003e_G</u> <u>esamtdokument.pdf</u>

Accident Prevention & Insurance Association - data sheets [BG-Merkblätter R 001-007]





PSCI Auditor Training 2019

Runaway Reaction Explosion

(taken from a presentation by Lamy Bao)

PSCI Questionnaire & observations

(Presentation from Dr. Stefan Gries Boehringer Ingelheim Corporate Center, Corp. EHS&S)

Speaker: Mr. Li Liu Boehringer Ingelheim Corporate China. EHS&S

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Investigation Report - Explosion in T-2 Labs

- Location: Jacksonville, Florida (USA)
- Incident: Explosion in Reactor due to runaway reaction
- 4 employees killed, 32 injured (including 28 from surrounding community
- Explosion force: Equivalent to 1,400 lbs of TNT (≈ 635 kg TNT)
- Causes:
 - Company did not recognize the worst credible scenario
 - No redundancy in cooling system
 - Inadequate pressure relief device



Reaction Hazards - Historical Data of Incidents

(Ref. Book: Chemical Reaction hazards by John Barton)

Following data was collected for 189 industrial incidents in UK involving thermal runaway reactions:

- 134 incidents were classified by processes, key ones are:
 - Polymerization (condensation): 64 (48%)
 - Nitration: 15 (11 %)
 - Sulphonation: 13 (10%)
 - Hydrolysis: 10 (7%)
 - Raw Materials Quality: 15 (11%)
 - **Others: 13%**
- 34 incidents were caused because there was no study done for reaction hazards



Reaction Hazards – Incidents by Causes

(Ref: Book: Chemical Reaction hazards by John Barton)

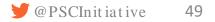
- 35 incidents were caused by mischarging of reactants or catalysts (29%)
- 32 incidents were caused by temperature control (27%)
- 25 incidents were caused by maintenance (21%)
- 17 incidents were caused by agitation (14%)
- 11 incidents were caused by human error (9%)



PSCI Questionnaire and Typical observations

Audit Questions Summary – Process Safety

Topic	Question summary
Process Safety	 76: Top 3 most hazardous process activities conducted at this facility 77: Process hazard assessment 78: Evaluated the impact of its operation on the community Evaluated the impact from the activities of neighboring businesses 79: Risk assessment for explosion of flammable liquids, vapors, powders, and gases 80: Preventive maintenance of safety relevant equipment. 81: Handling compressed gases safely 82: Bulk chemical handling procedures 83: Safety measures around direct fire equipment (e.g. boiler, incinerators, ovens etc.)



77	Does the facility perform Process Hazard Assessment		
	(PHA)? Aim is to identify processes or operations that could present significant risks in case of deviation (exothermic reactions, use of flammable, combustible or toxic materials, processes involving extreme temperatures or pressures).	 Collection of process information (process safety data, design information, operating parameters, and equipment specifications) 	
		• Hazard evaluations capturing significant risks during process development, preliminary engineering, and upon completion of process design?	
		 Sizing of pressure vessels and relief devices according to appropriate codes and standards? 	
		 Flammable storage areas separate from production and well managed? 	

No safety data for any chemical reaction are available (example: heat of reaction, adiabatic temperature rise, decomposition temperature,...)

The auditee has made some improvement to collect process safety data and to conduct PHA for high sophisticated chemical reaction (nitration, oxidization, hydrogenation etc.) running at site. Nevertheless the interpretation of this data and the transfer into safety measures for the production is not always reliable.

Basic safety data for chemical processes are available from the Development report. However data are archived and in case of changes these data are not any more reconsidered, since there is no systematic approach in place to cover chemical safety data in a change control system.



Most of the vent pipes coming from safety valves or rupture disks have at least 3 ninety degree angles. Therefore there is no evidence about the pressure profile inside the venting pipe. This leads to back pressure build up in case of activation with a certain risk for pipe bursting.

The reactor where the bromination takes place misses a safety valve or rupture disc respectively. Furthermore the adiabatic reaction heat is not known.

The explosion vent of the fluid bed dryer in the Bromhexine clean rooms is venting into the cleanroom.

In the chemical production building, the venting pipes of the safety valves end close to the floor in the production room. Taking into consideration the highly hazardous nature of the ingredients (e.g. Oleum, CO, SO₃) this may lead to fatal accidents in case of a pressure relief.



79 Does the facility perform risk assessment related to the explosion of <u>flammable liquids</u>, <u>vapors</u>, <u>powders</u>, <u>and gases</u> in processing operations (including storage, transfer and charging)?

Does it include the following steps?

- Assessment of the hazards (Minimum Ignition Energy, Kst classification rating, Impact sensitivity etc.) of the handled combustible dusts and powders
- Hazardous area classification (zones according EU-ATEX and Classes according to US-NFPA) ...
- Installation of special electrical equipment for flammable vapors, gases, combustible dusts, ...
- Periodic testing of grounding and bonding circuits, lightning arresters, and electrical distribution equipment?
- Maintenance/calibration done for critical safety equipment (e.g. sensors, instruments, valves, interlocks, reactors, condenser etc.) at suitable intervals.
- Assessment of the hazards due to mechanical ignition sources?
- Installation of special electrical equipment for flammable vapors, gases, combustible dusts, and wet areas?
- Periodic testing of grounding and bonding circuits, lightning arresters, and electrical distribution equipment?
- Maintenance/calibration done for critical safety equipment (e.g. sensors, instruments, valves, interlocks, reactors, condenser etc.) at suitable intervals.
- Assessment of the hazards due to mechanical ignition sources?



Safety data like MIE, St Class etc. are available for most of the finished products (API). No data is available for isolated intermediates. Hence it could not be proven if the Fluid Bed Drying of intermediates can be done safely.

The company has not assessed the hazards (Minimum Ignition Energy, K_{st} classification rating, Impact sensitivity etc.) associated with combustible dusts and powders being handled in various operations at site.

At the installations in the production area stainless steel clamps were installed instead of using copper wires for grounding and bounding. No evidence was provided showing that this type of bounding grounding is as safe and effective as copper wires.



The Customer product is received in packaging, treated in anti-static agents and the specifications for the finished product require it to be packaged in liners that are treated with anti-static agents. However, the material handled in the intermediate steps is not treated with anti-static agents. Site personnel assume that the minimum ignition energy is low enough to warrant this type of packaging if the incoming and finished product are packaged in anti-static treated liners.

There is no gas detector near the ethanol recovery device at VB1 workshop, no O2 detector at centrifuges which used N2.

In the production plant, grounding points and grounded piping are installed. A detailed SOP for working in Ex-zones is available and trained.

But an instruction, how to ground mobile equipment (e.g. solvent drums) is not included in this SOP.

An Ex light in the hydrogenation room was labeled as "Ex ed IIB T4", which was not the proper type for hydrogen environment.

80	Describe how the facility ensures preventive	Pressure safety relief valves/rupture disks
	maintenance of safety relevant equipment.	Bonding/earthing systems
		 Mass transfer systems (e.g. piping systems)
		Pressurized vessels
		Explosion prevention system (e.g., prevention of static electrical discharge)
		 Is there emergency power supply for relevant equipment?

Anti-static bridge connection of pipes for transporting flammable chemicals is very rusty in Building A-6.

Most of the P+IDs presented during the audit where not up to date. Furthermore the guidelines of ISO14617 regarding the symbols are not followed.

P+IDs should always be up to date, showing the "as build" situation to avoid any risk due to mistaken identity of any component of an equipment.

81	, i i i i i i i i i i i i i i i i i i i	Inspection and approval before acceptance of delivery?
	compressed gases safely that includes:	Storage in a segregated area designed for compressed gases?
		Separation or barriers to manage compatibility issues?
		Gas classification labeling?
		Regulator, hose and flexible connection inspections?



PSCI Questionnaire

82	Has the facility developed and implemented bulk chemical handling procedures that include:	Not applicable Specific unloading and loading procedures? Identification sampling before unloading? Hose inspection? Fire protection? Spill control measures (dike or bund area)?
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Storage of Oxalyl Chloride is done under "normal" conditions (Hyderabad room temperature in the warehouse).

As of the "Tech Pack" information, the storage temperature should not exceed -10°C. Even if there are some newer SDS available that storage at middle European room temperature range (max. 25°C) might be sufficient, the company could not show evidence that the change of storage conditions was assessed.

The bulk unloading process needs improvement. The unloading area is asphalt but no defined retaining volume in case of any spillage is provided.



83	What are the safety measures around direct fire equipment (e. g. boiler, incinerators, ovens etc.)?	
	Consider gas accumulation, steam overpressure	

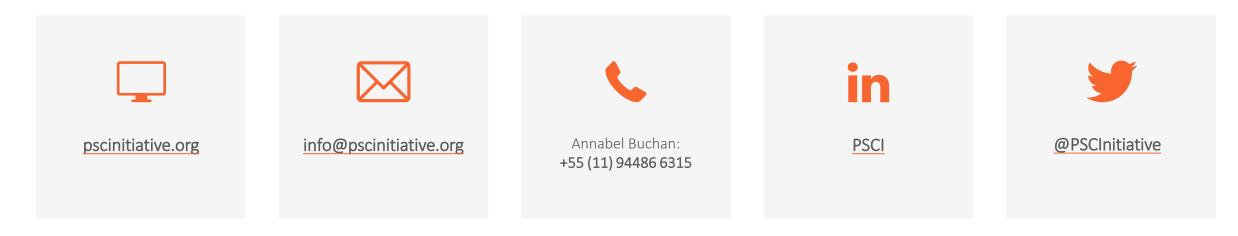
In the Building B, Water For Injection (WFI) system, the clean steam generator operates at 65 psig with a safety relief valve venting directly to the room. In the case of activation, 155°C steam would be released and fill the room.







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About the Secretariat

Carnstone Partners Ltd is an independent management consultancy, specialising in corporate responsibility and sustainability, with a long track record in running industry groups.



